

# Dynamically Load-balanced $p$ -adaptive Discontinuous Galerkin Methods using Charm++

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# Outline

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- Background
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- DG Discretization Formulations
  - Weak formulation
- Adaptive Strategies
  - Error indicator based  $p$ -adaptation
  - Protective layer refinement
- Computation Process
- Numerical Results
- Conclusions

# Quinoa

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- Computational tools for fluid dynamics
- Written in modern C++
- Production-style, rigorously tested
- Numerical solver for single-material and multi-material hydrodynamics
- Asynchronous, distributed-memory parallel programming
- Fully unstructured tetrahedral mesh support
- Dynamic load balancing and automatic object migration using Charm++
- Open source:  
<https://github.com/quinoacomputing/quinoa>

# Governing Equations

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- The compressible Euler equations can be represented as

$$\frac{\partial \mathbf{U}}{\partial t} + \frac{\partial \mathbf{F}_k}{\partial x_k} = 0$$

where

$$\mathbf{U} = \begin{bmatrix} \rho \\ \rho u_i \\ \rho E \end{bmatrix}, \quad \mathbf{F} = \begin{bmatrix} \rho u_k \\ \rho u_i u_k + p \delta_{ik} \\ u_{ik} (\rho E + p) \end{bmatrix}$$

- The pressure can be evaluated according to

$$p = (\gamma - 1)\rho \left( E - \frac{1}{2} u_i u_k \right)$$

where  $\gamma$  is the ratio of specific heats

# Discontinuous Galerkin Formulation

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## 2.1 Weak formulations

- The weak formulation can be obtained by multiplying test function  $W$  and performing integration by parts,

$$\int_{\Omega} \frac{\partial U_h}{\partial t} W_h d\Omega + \int_{\Gamma} F_k(U) n_k W_h d\Gamma - \int_{\Omega} F_k(U) \frac{\partial W_h}{\partial x_k} d\Omega = 0$$

- Assume our high order solution within the cell is represented as,

$$U_h(x, t) = \sum_{j=1}^N u_j(t) B_j(x)$$

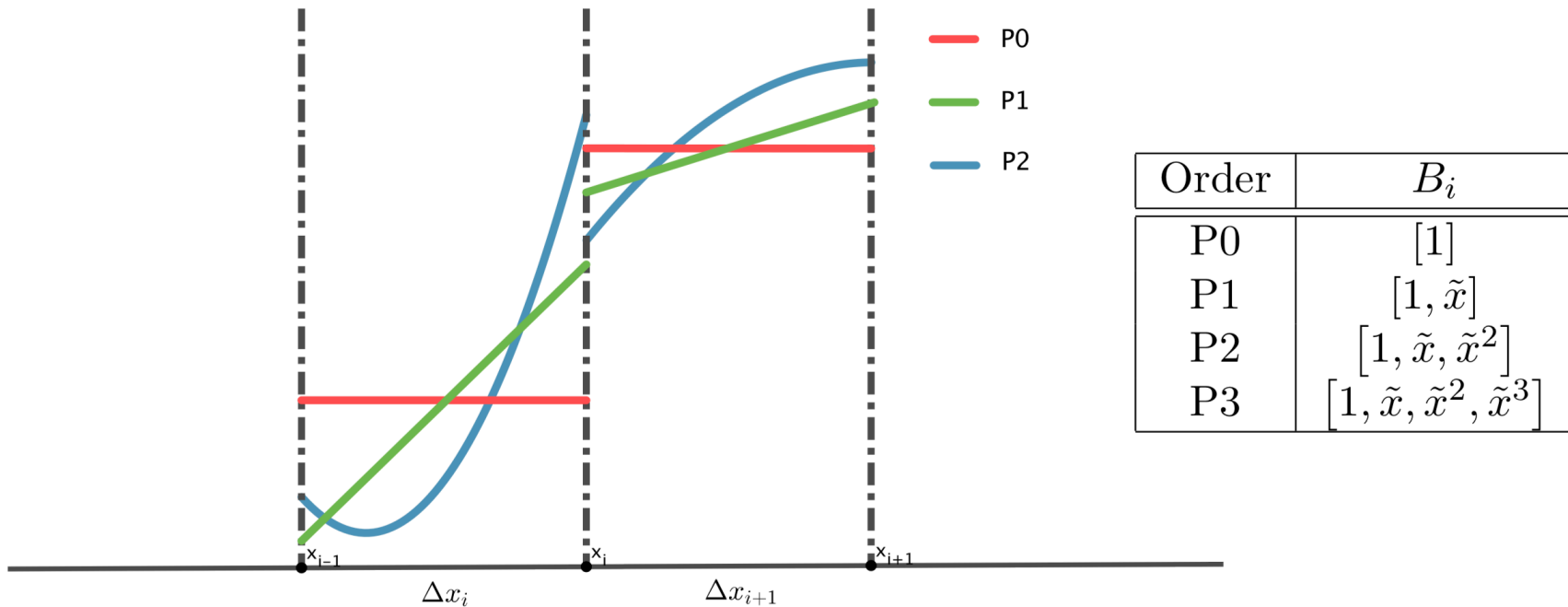
- Apply the solution equation to the above formulation,

$$\left( \int_{\Omega_e} B_i B_j d\Omega \right) \frac{du_j}{dt} + \int_{\Gamma_e} F_k(U_h) n_k B_i d\Gamma - \int_{\Omega_e} F_k(U_h) \frac{\partial B_i}{\partial x_k} d\Omega = 0, 1 \leq i \leq N$$

# Discontinuous Galerkin Formulation

## 2.1 Weak formulations

- The DG solution:  $U_h(x, t) = \sum_{j=1}^N u_j(x) B_j(x)$



# Adaptive Strategies

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## 3.1 Error indicator based $p$ -adaptation

- Use a posteriori local error indicator to determine where the order of element solution should be refined or coarsened
- The spectral decay indicator is defined as

$$\eta_k = \frac{\int_{\Omega} (\rho_p - \rho_{p-1})^2 d\Omega}{\int_{\Omega} \rho_p^2 d\Omega}$$

Where  $\rho_p$  and  $\rho_{p-1}$  represent the numerical density with the polynomial order of  $p$  and  $p - 1$ .

- After evaluating adaptive indicators, the following adaptation criterion is used to determine  $p$ -refinement or coarsening:

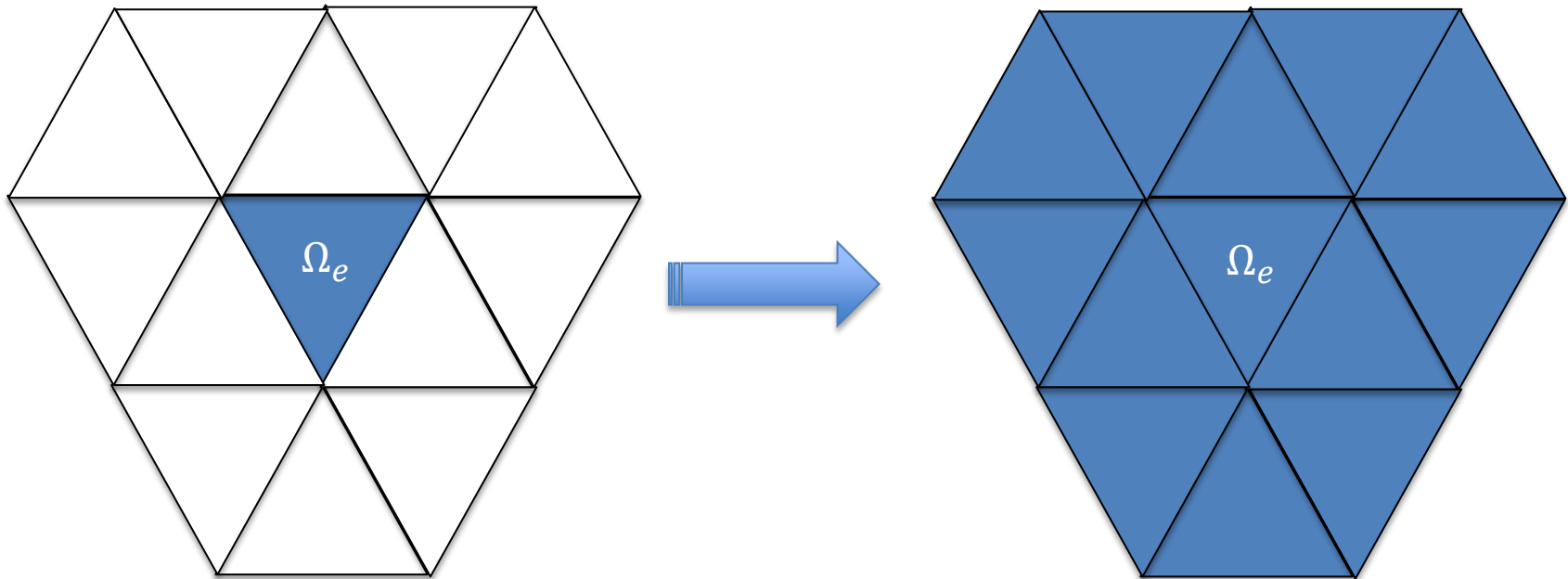
$$\begin{cases} \eta_k \geq \varepsilon_H \implies \text{Refine if } p_k < p_{max} \\ \eta_k < \varepsilon_L \implies \text{Coarse if } p_k > p_{min} \end{cases}$$

Where  $\varepsilon_H$  and  $\varepsilon_L$  are user-input thresholds ( $\varepsilon_H > \varepsilon_L$ ). Both thresholds are case-dependent parameters.

# Adaptive Strategies

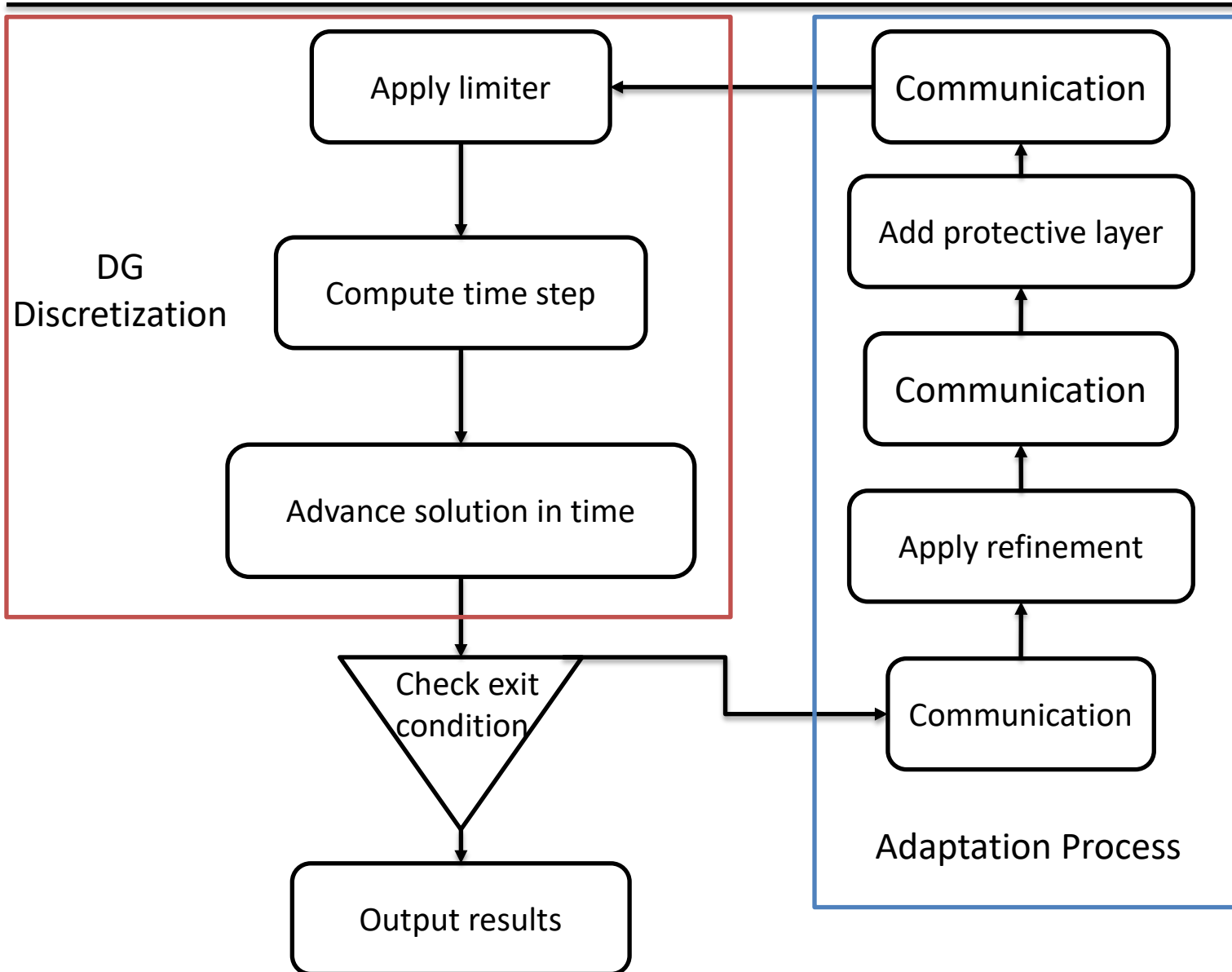
## 3.2 Protective layer refinement

- By adding this protective layer, refine all the nodal neighboring elements of the refined element in  $\Omega_e$



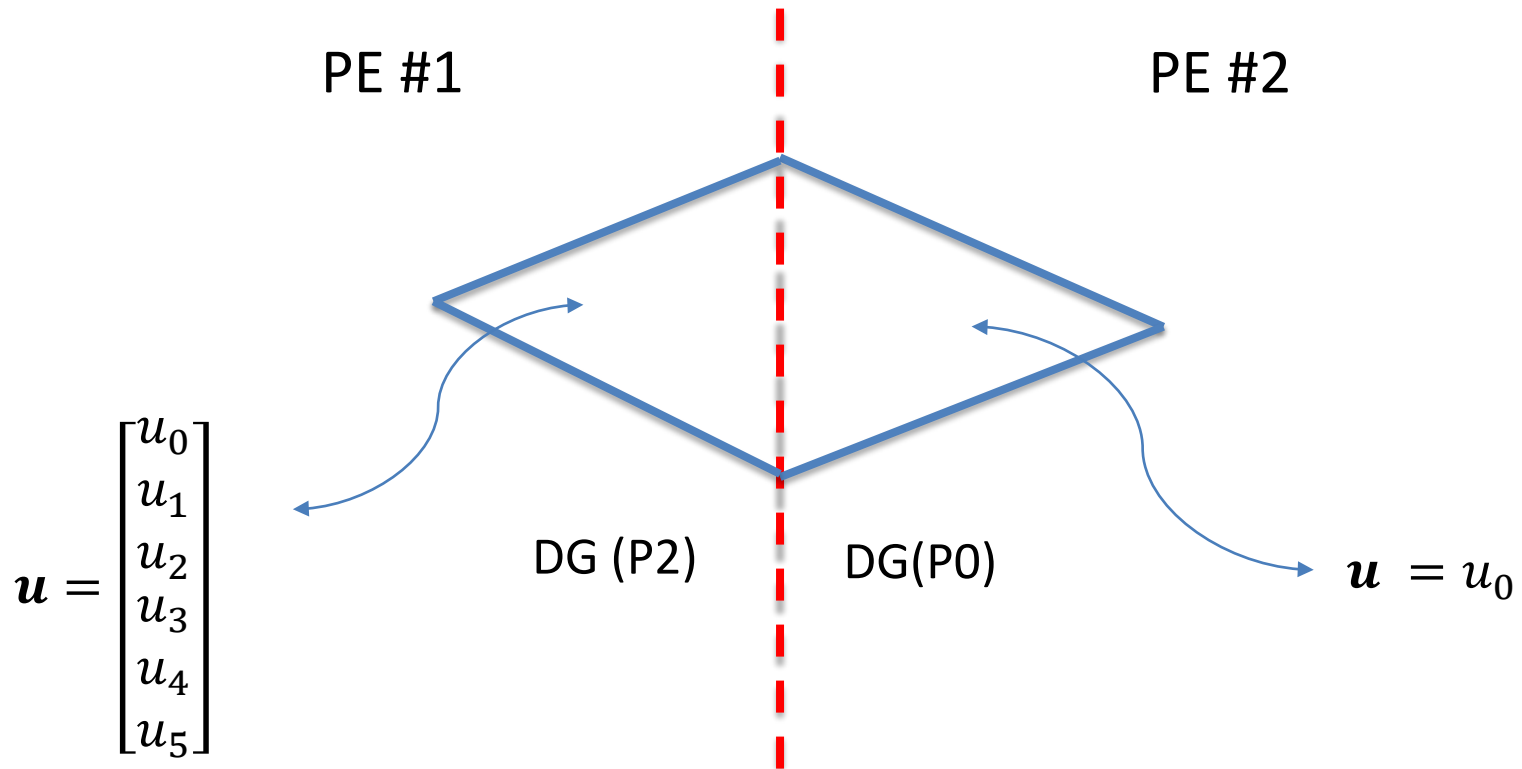


# Computation Process



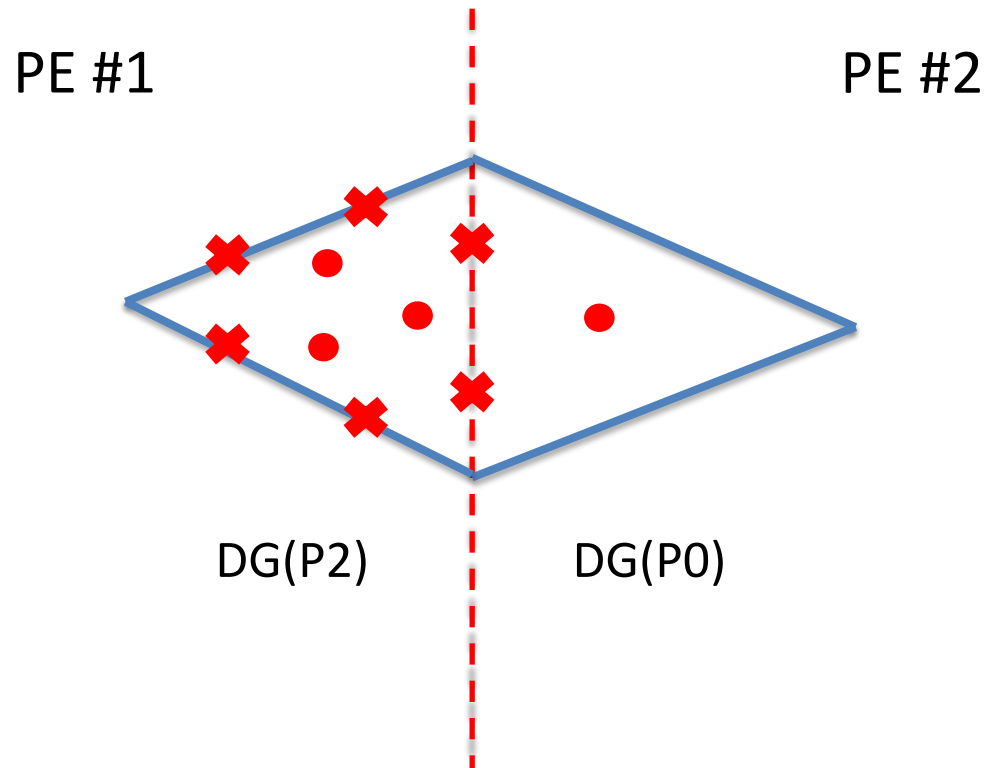
# Adaptive Strategies

## 3.3 Sources of unbalanced load distribution



# Adaptive Strategies

## 3.3 Sources of unbalanced load distribution



⇒ *Dynamic Load Balancing*

# Numerical Results

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## 4.1 Sod shocktube problem

- The initialization condition is given as

$$(\rho, p, u)_L = (1.0, 1.0, 0.0)$$

$$(\rho, p, u)_R = (1.0, 1.0, 0.0)$$

- The mesh with 11200 tetrahedra is used here

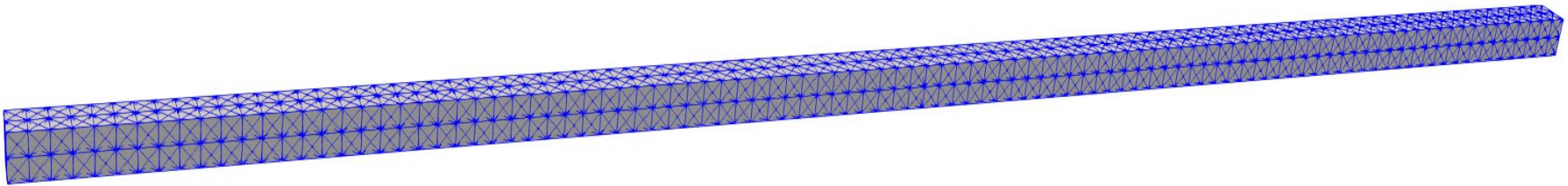


Fig. 1 Mesh for sod shocktube

# Numerical Results

## 4.1 Sod shocktube problem

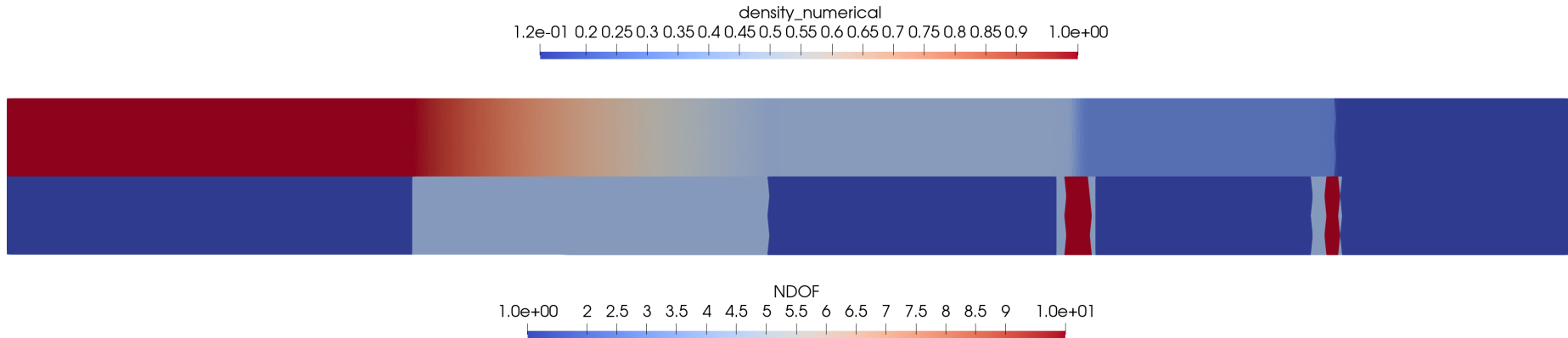


Fig. 2 Numerical distribution for sod shocktube

# Numerical Results

## 4.1 Sod shocktube problem

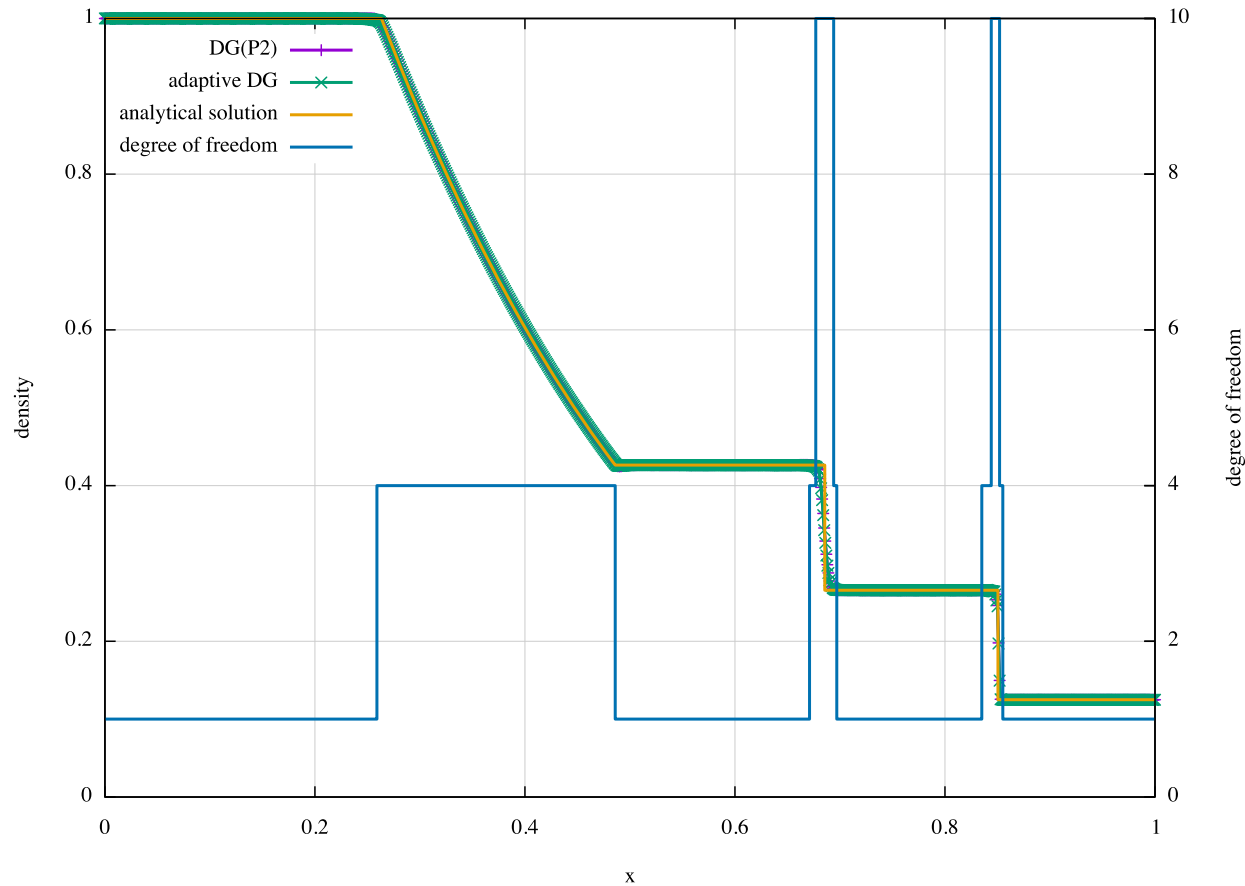


Fig. 3 Numerical distribution for sod shocktube in 1D

# Numerical Results

## 4.1 Sod shocktube problem

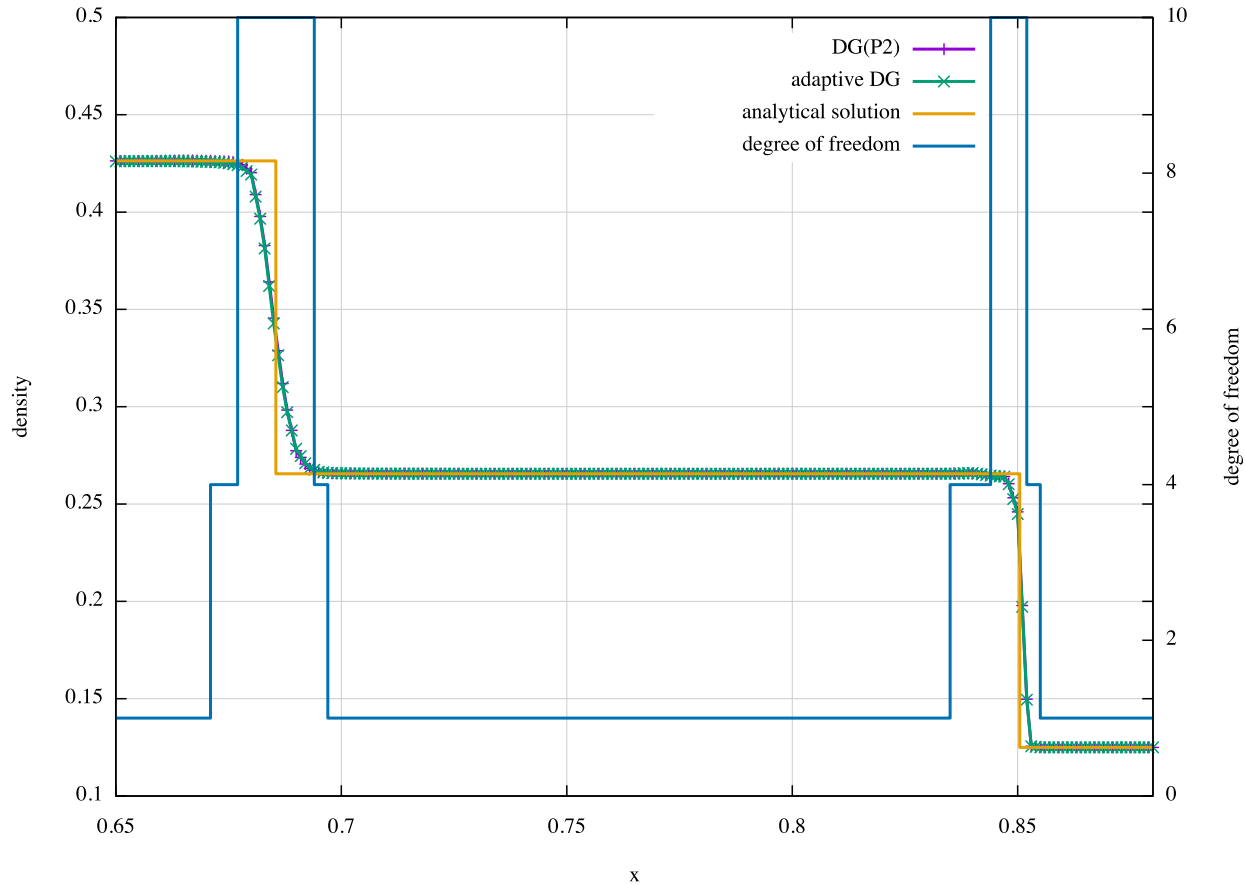


Fig. 4 Numerical distribution for sod shocktube near discontinuities

# Numerical Results

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## 4.1 Sod shocktube problem

Case	Configuration	Wall-clock time (m:s)	Speedup relative to case 2
1	128 cores, 128 partitions, DG(P2)	36:44	
2	128 cores, 128 partitions, $p$ -adaptive DG	33:52	
3	128 cores, 426 partitions, $p$ -adaptive DG	16:56	2.0x
4	128 cores, 426 partitions, $p$ -adaptive DG with load balancer	16:17	2.1x

Table 1. Wall-clock time table for sod shocktube



# Numerical Results

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## 4.2 Sedov blast problem

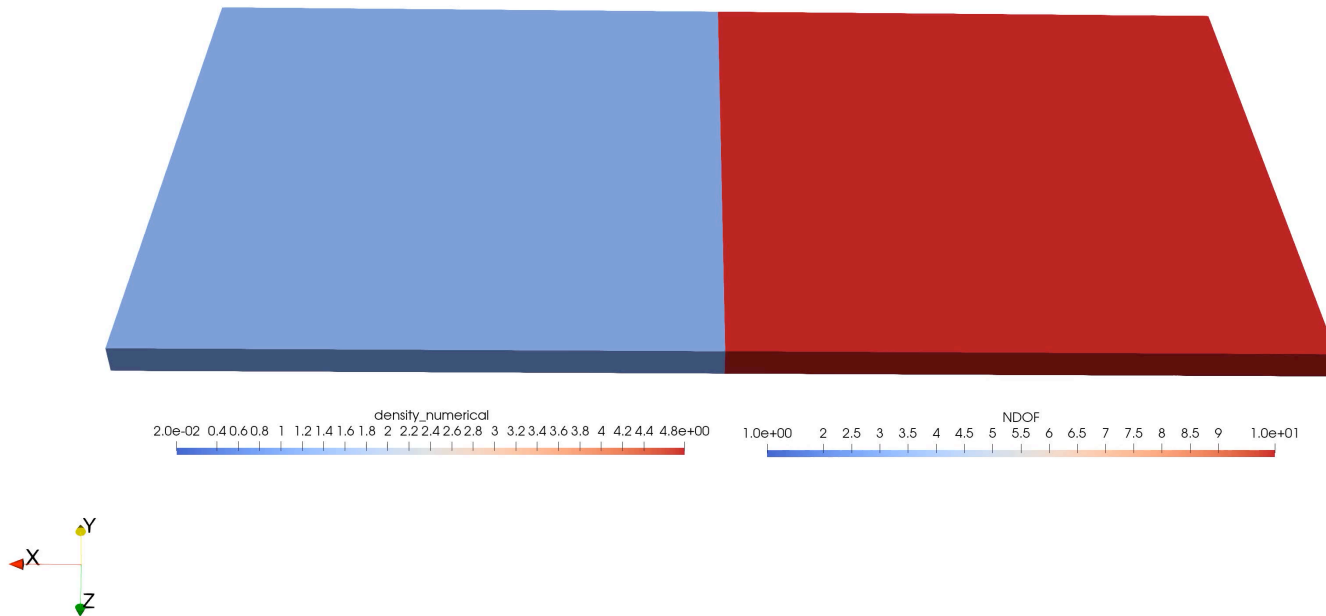
- Sedov blast testcase describes the flow with a strong spherical shock wave.
- The initialization condition is given as

$$\begin{aligned}u_x &= 0 \\ \rho(x_i) &= 1 \\ p &= \begin{cases} 783.4112 & \text{if } x_i < 0.05 \\ 0 & \text{otherwise} \end{cases}\end{aligned}$$

- The mesh with 29k tetrahedra is used here
- The goal of this testcase is to assess the capability to capture the strong discontinuities.

# Numerical Results

## 4.2 Sedov blast problem



# Numerical Results

## 4.2 Sedov blast problem

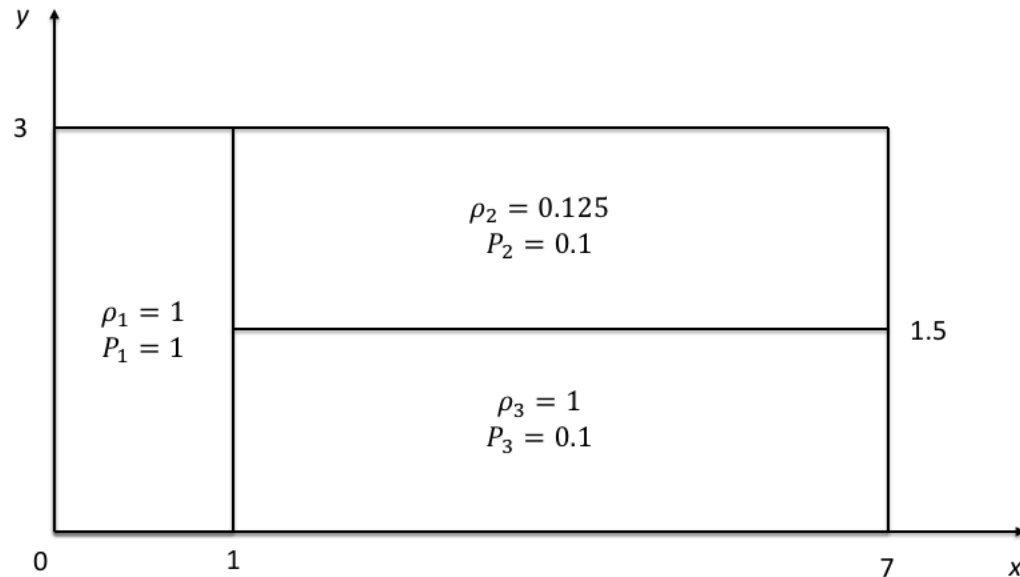
Case	Configuration	Wall-clock time (h:m:s)	Speedup relative to case 3
1	64 cores, 64 partitions, DG(P2)	5:00:29	
2	64 cores, 319 partitions, <i>DG(P2)</i>	5:26:5	
3	64 cores, 64 partitions, <i>p</i> -adaptive DG	3:13:29	
4	64 cores, 319 partitions, <i>p</i> -adaptive DG	1:35:21	2.0x
5	64 cores, 319 partitions, <i>p</i> -adaptive DG with load balancer	1:21:42	2.4x

Table 2. Wall-clock time table for Sedov blast at  $t = 0.01$

# Numerical Results

## 4.3 Triple point problem

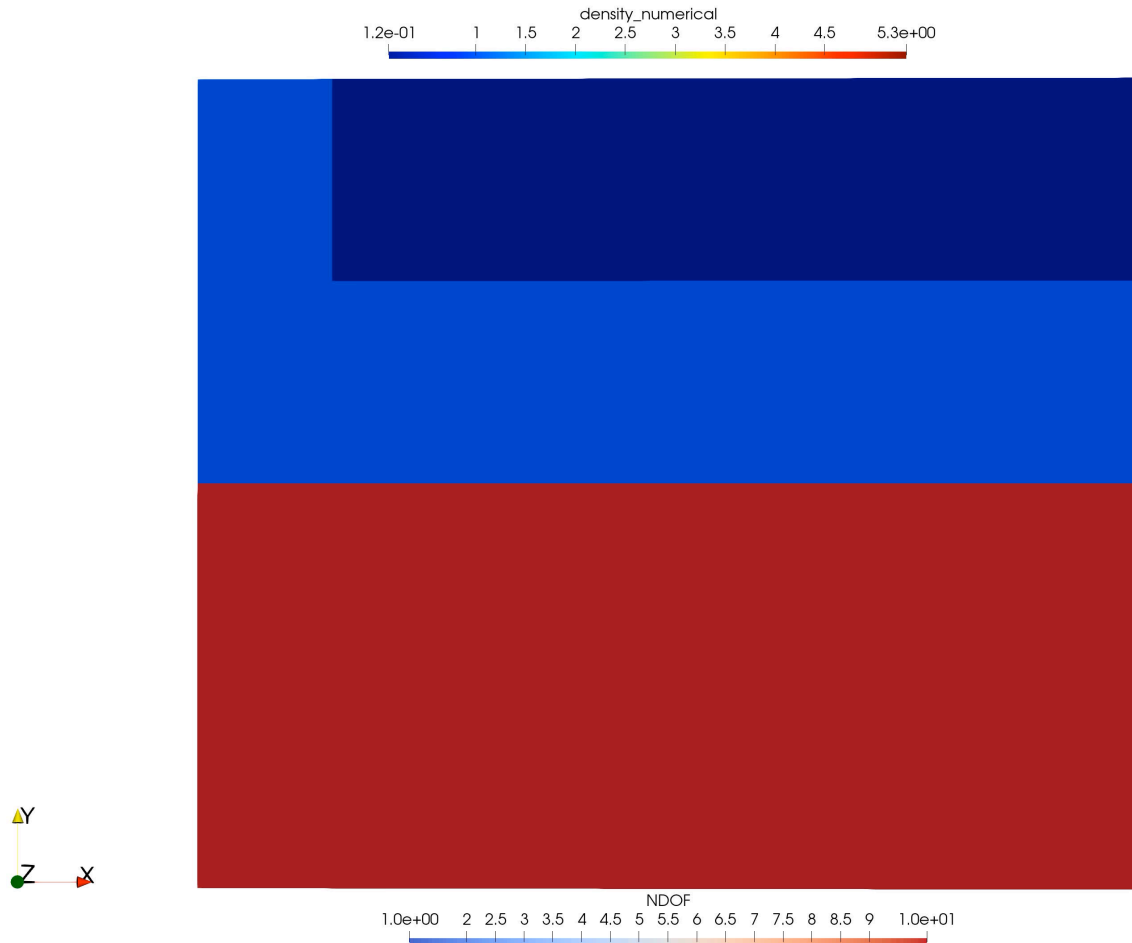
- The triple point problem is three-state two-dimensional Riemann problem
- The initialization condition is given as



- The mesh with 687085 tetrahedra is used here

# Numerical Results

## 4.3 Triple point problem



# Numerical Results

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## 4.3 Triple point problem

Case	Configuration	Wall-clock time (h:m:s)	Speedup relative to case 3
1	32 cores, 32 partitions, DG(P2)	5:17:48	
2	32 cores, 32 partitions, $p$ -adaptive DG	6:16:12	
3	32 cores, 319 partitions, $p$ -adaptive DG	3:37:43	1.7x
4	32 cores, 319 partitions, $p$ -adaptive DG with load balancer	2:4:29	3.0x

Table 3. Wall-clock time table for triple point problem at  $t = 1$

# Numerical Results

## 4.3 Triple point problem

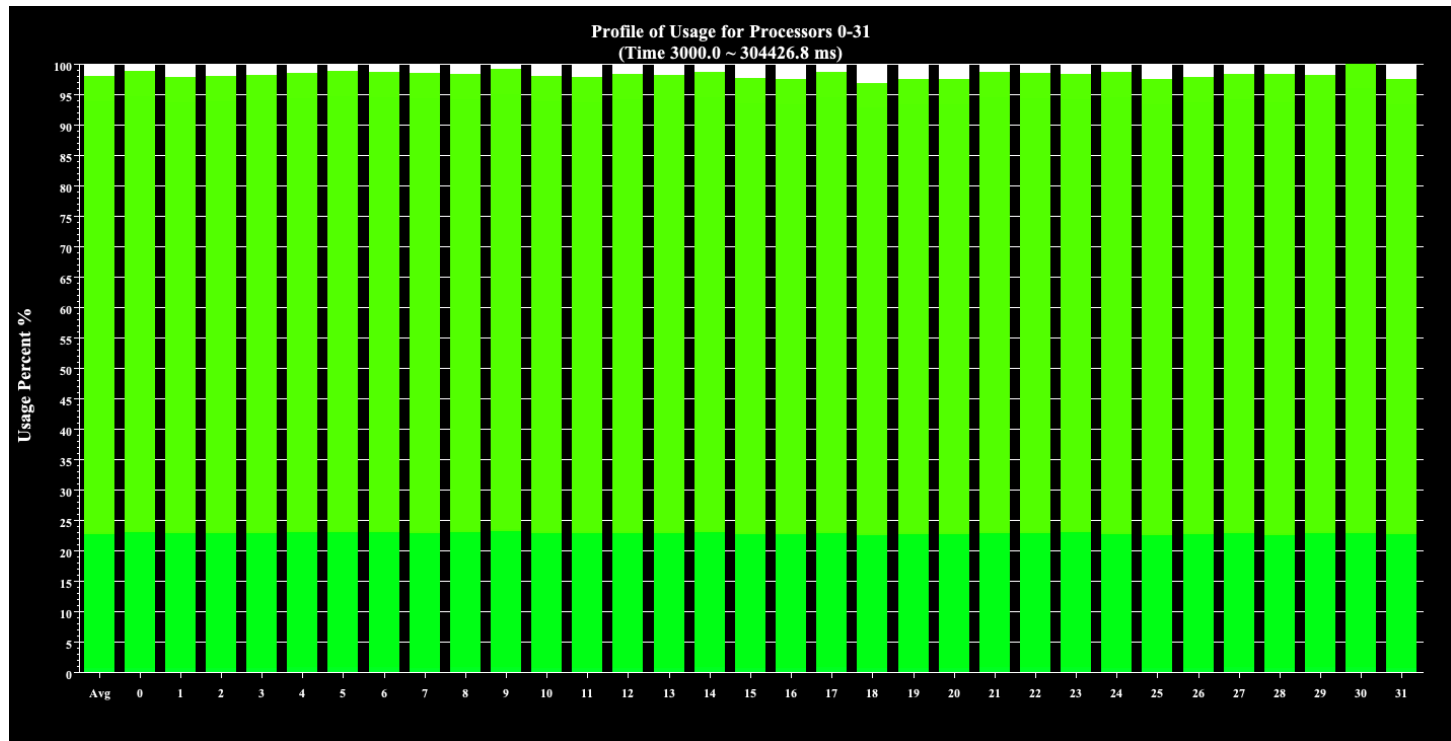


Fig. 5 Usage profile for DG(P2) with 32 cores

# Numerical Results

## 4.3 Triple point problem

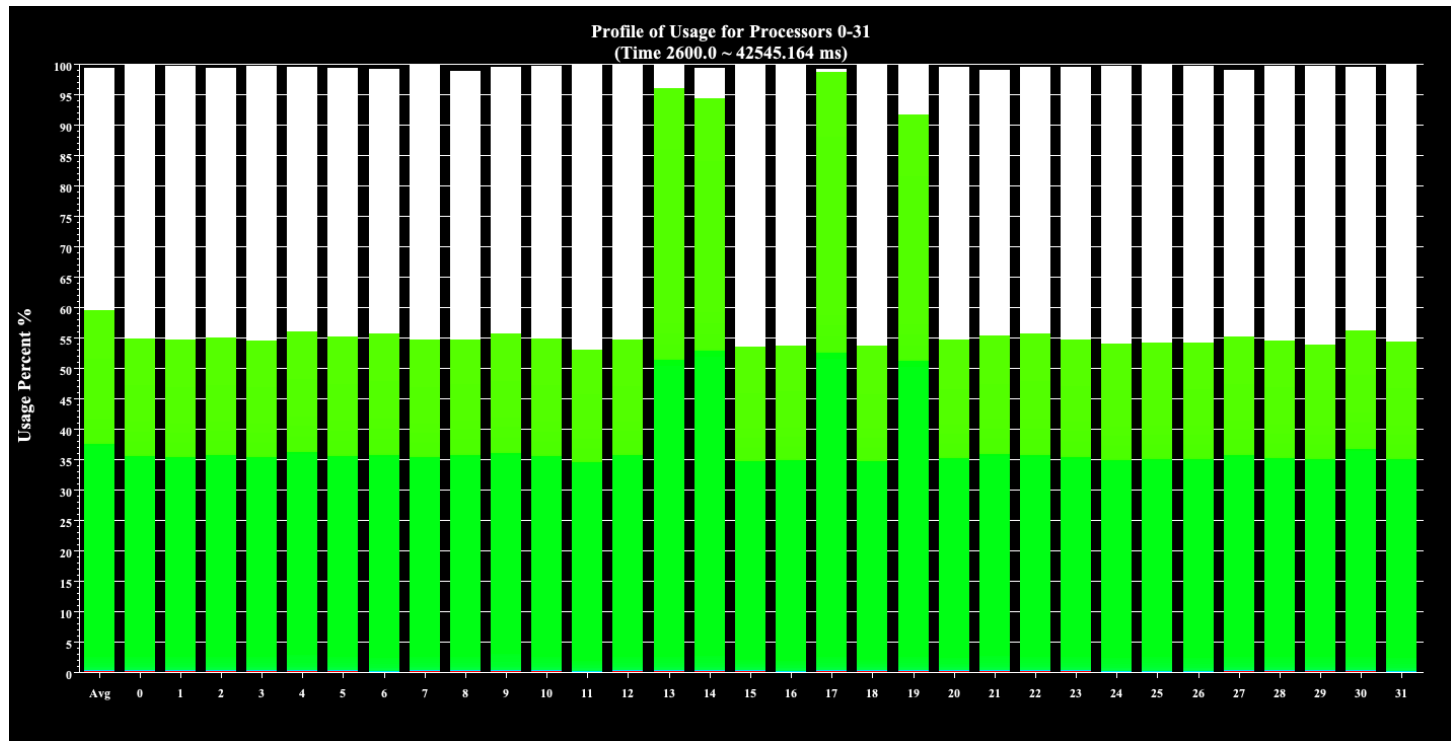


Fig. 6 Usage profile for  $p$ -adaptive DG with with 32 cores



# Numerical Results

## 4.3 Triple point problem

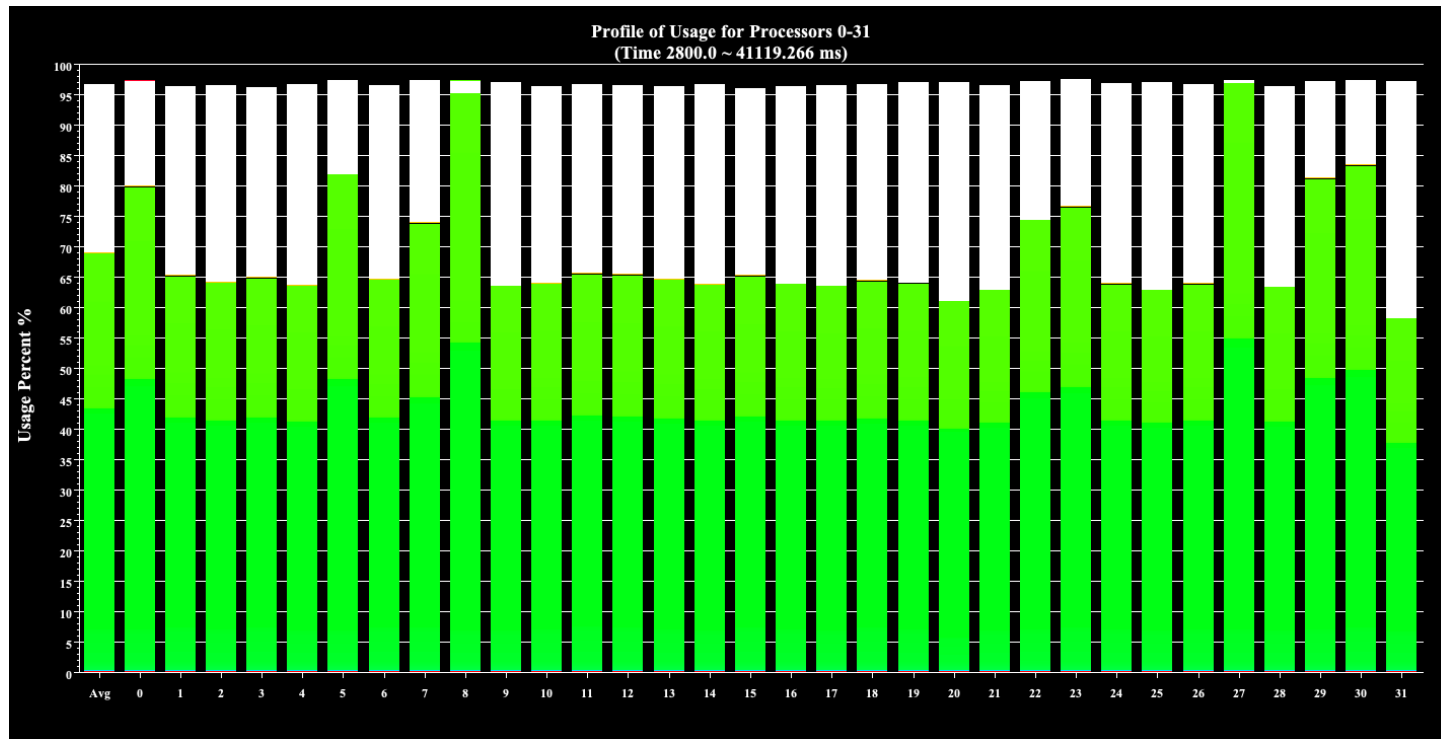


Fig. 7 Usage profile for  $p$ -adaptive DG with over-decomposition

# Numerical Results

## 4.3 Triple point problem

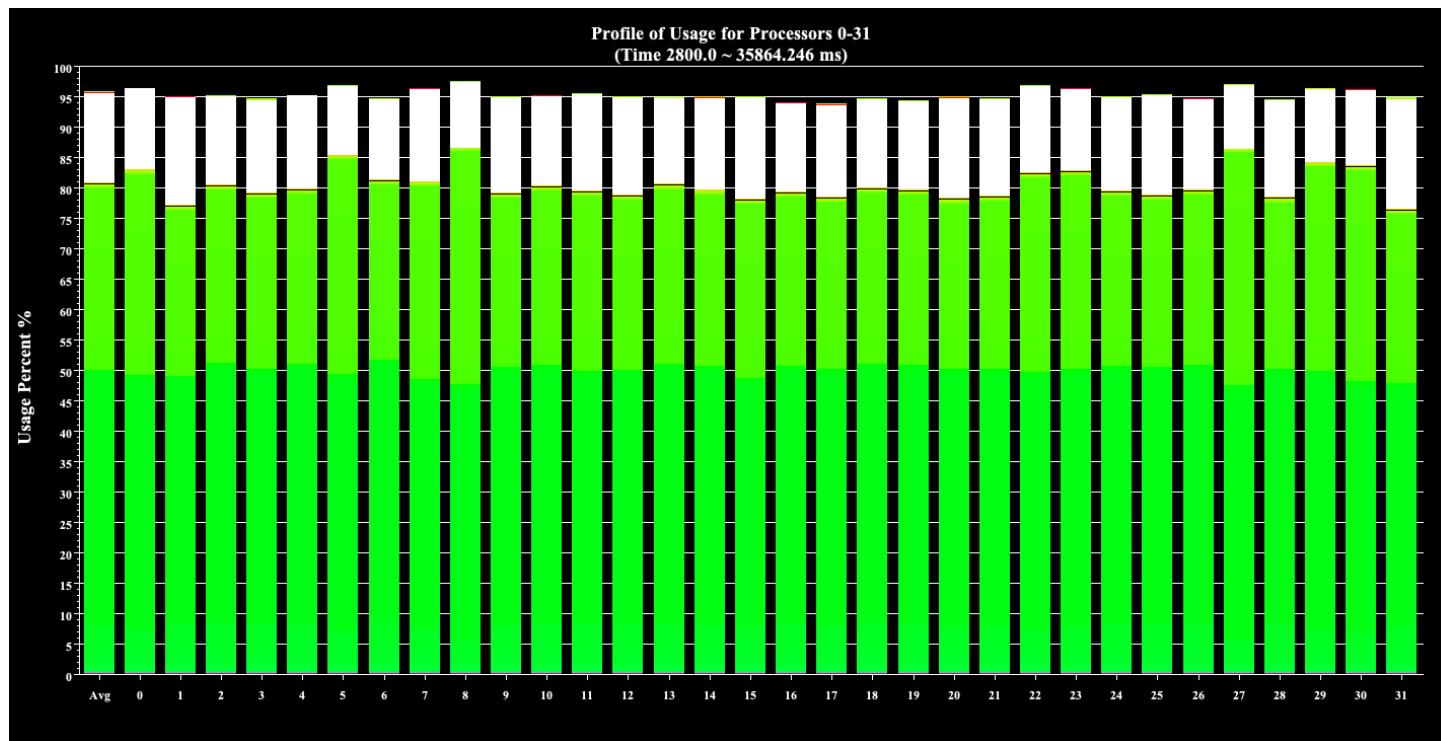


Fig. 8 Usage profile for  $p$ -adaptive DG with load balancer

# Summary

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- A  $p$ -adaptive DG method is developed.
- The developed adaptive method introduces unbalanced load distributions.
- The adaptive scheme combined with load balancing techniques significantly increase the computation efficiency.
- More complex numerical methods will be implemented within this parallel structure to maximize the benefits of dynamic load balancing technique.